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# Imaging spectroradiometer for HF laser studies

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## ABSTRACT

We discuss a non-intrusive diagnostic for mixing, species concentration, and optical gain for HF chemical lasers. The instrument is based on hyperspectral imaging using a low order Fabry-Perot interferometer. The basic theory behind this technology is described and several applications to a chemically reacting flowfield are presented

**Keywords:** chemical laser diagnostics, hyperspectral imaging, reactive flows

## 1. INTRODUCTION

Certain gas phase chemical reactions form product states that have inverted population distributions. For example, the  $F + H_2$  reaction produces  $H + HF(v,J)$  where partial inversions exist between many rovibrational levels. Mixing of the reacting gas streams in a chemical laser is a key parameter for producing efficient devices.<sup>1-3</sup> This was recognized soon after the first laser demonstrations, but effective diagnostics did not exist that could survive corrosive environments or did not perturb the flows. Measurements of mixing, vibrational and rotational temperatures, small signal gain, and spectral output were difficult and often inaccurate. Even though the HF chemical laser concept is more than 30 years old, there are still important scaling parameters for which there are no effective diagnostics. In 1978 Rapagnani and Davis demonstrated that laser induced fluorescence could be used as a diagnostic for mixing in chemical laser nozzles, and they later developed methods for studying both hot flow and cold flow mixing.<sup>4,5</sup> In this paper we discuss a new diagnostic for reactive mixing in chemical lasers. Using a device we call the Adaptive Infrared Imaging Spectroradiometer (AIRIS) we have developed methods for examining mixing of F and  $H_2$  flows and for determining spatially resolved maps of population inversions between selected HF rovibrational levels.

### 1.1 Background

The AIRIS technology was developed at Physical Sciences Inc. (PSI) to address the need for a moderate resolution, rapidly tuned imaging spectrometer for a variety of applications. Our technology is based on Fabry-Perot (F-P) interferometry. Fabry-Perot devices rely upon multiple beam interference between two highly reflecting mirrors to produce an interference pattern that contains spectral information about the light source being probed. If the light source is collimated with a lens, then the resulting interference pattern is usually a series of concentric rings, each representing a different order of the interference. This is illustrated in Fig. 1.

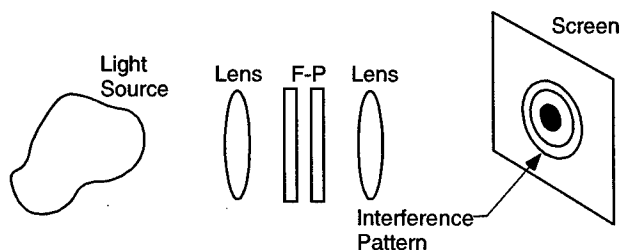


Fig. 1: Typical arrangement for F-P interferometers.

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Jacquino<sup>6</sup> described an important application of the F-P with the introduction of the center spot technique. He showed that if one placed a pinhole in front of a detector that restricted the detector to view only a small portion of the center spot of the interference pattern, then one could use the F-P as a spectrometer by recording the transmitted light as a function of the distance between the F-P mirrors. Davis and co-workers<sup>7</sup> used this approach to obtain the first measurements of the collisional broadening coefficient for oxygen on the atomic iodine laser line, crucial data for COIL. This type of spectrometer offers several advantages including: high throughput, high spectral resolution, and compact size.

### 1.1.1 Basic concepts

The *AIRIS* instrument comprises an IR focal plane array (FPA) coupled to a Fabry-Perot interferometer through imaging optics. In this configuration the interferometer operates as a tunable interference filter, selecting the wavelength viewed by the FPA. In this section we describe the theoretical basis for the development of the interferometer as well as the consequences and advantages of low-order operation.

In a Fabry-Perot interferometer light is selectively transmitted by constructive interference through the faces of two partially-reflecting parallel mirrors. Light is transmitted for wavelengths which satisfy the expression:

$$\lambda_t = \frac{2\ell}{m} \cos \theta \quad (1)$$

where

- $\ell$  = mirror spacing
- $m$  = order of interference
- $\theta$  = incidence angle
- $\lambda_t$  = transmitted wavelength.

A range of mirror spacings, incidence angles, and orders will all lead to the transmission of a single wavelength. The free spectral range,  $\Delta\lambda_{\text{FSR}}$ , determines the range of wavelengths transmitted between successive orders of interference:

$$\Delta\lambda_{\text{FSR}} = \frac{\lambda_{\text{max}}}{m_{\text{max}} + 1} \quad (2)$$

where  $m_{\text{max}}$  is the order in which  $\lambda_{\text{max}}$  is transmitted for paraxial rays.

The finesse,  $F$ , determines the spectral resolution of the interferometer, which is always a fraction of the free spectral range:

$$\Delta\lambda_{1/2} = \frac{\Delta\lambda_{\text{FSR}}}{F} \quad (3)$$

The elements which define the finesse of the interferometer arise from the reflectivities of the mirrors as well as "defects" in their configuration, such as mirror flatness and parallelism. The total finesse of the interferometer is obtained from the inverse root mean square sum of each finesse component. For practical operation in the infrared, the defect finesse is the limiting factor in determining total finesse. The total finesse can seldom be greater than approximately 30 to 50 due to these limitations.

The interferometer field of view (focal length and detector element size) determines the range of angles incident and detected by the system. Equation (1) shows that a range of incidence angles and interference orders will allow transmission of a common wavelength through the interferometer for a single mirror spacing. The aperture finesse defines the degradation in spectral resolution within a single order due to this effect:

$$F_A = \frac{2}{m(\Delta\theta)^2} \quad (4)$$

As a consequence of Eq. (4), the field of view over which an acceptable finesse can be obtained increases as the interferometer is operated in lower orders. When using IR focal plane arrays, system instantaneous fields-of-view ranging from 6 to 15 deg are generally consistent with an overall finesse of 35.

The short wavelength AIRIS used in this work contains two, custom mirrors with high reflectivity in the 2.0 to 3 micron spectral region. The 38 mm diameter mirrors were fitted with specialized gold pads that form four capacitors that are used to measure and monitor the separation and alignment of the two mirrors in the Fabry-Perot configuration. A photo of the short wavelength AIRIS head is shown in Fig. 2.



Fig. 2: Photo of AIRIS device used to probe HF(v,J) emission.

## 2. EXPERIMENTS

### 2.1 Calibrations

Initial testing of the AIRIS system was conducted using a Fourier Transform Infrared (FTIR) spectrometer. The AIRIS head was positioned inside the FTIR, and the FTIR provides a tunable, narrow spectral band of light that can be used as an essentially monochromatic source for AIRIS calibrations. This quasi-monochromatic beam ( $0.5$  to  $2\text{ cm}^{-1}$ ) passed through the AIRIS and the transmitted intensity was monitored as a function of the wavelength of the source and the mirror separation in AIRIS. Recall that in a Fabry-Perot interferometer the wavelength of the transmitted light is a function of the mirror separation. We performed initial calibration of the AIRIS by systematically setting the mirror separation while recording the transmitted intensity as the wavelength of the light passed by the FTIR was scanned. As the wavelength of the light incident on the AIRIS passed through cavity resonances, transmission peaks of the consecutive orders were observed. A typical spectrum is shown in Fig. 3.

### 2.2 Chemical HF(v,J) production

We used a high power Microwave Driven Jet (MIDJet™) device to produce the F atoms. MIDJet™ is an electrodeless discharge so that corrosion is not an issue. It has been applied to numerous feedstock gases including SF<sub>6</sub>, O<sub>2</sub>, He, Cl<sub>2</sub>, NF<sub>3</sub>, and air. The source gas and diluent are fed into the discharge region of MIDJet™ through a series of sonic injection nozzles. The design of these injectors stabilizes the discharge along the axis of the MIDJet™ chamber and enables the device to operate over a large range of pressures and flow rates. Both sonic and subsonic exit nozzles can be used to cover a wide range of exit conditions. The supersonic exit nozzle isolates the conditions inside the MIDJet™ chamber for flow conditions downstream of the nozzle.

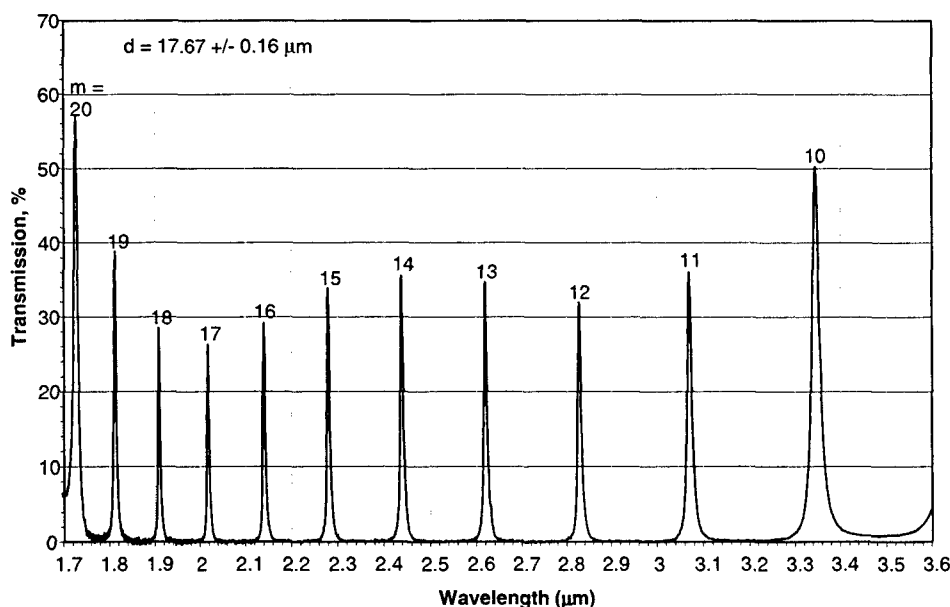


Fig. 3: AIRIS transmission as a function of the wavelength of incident light for a mirror separation of  $17.67 \pm 0.16 \mu\text{m}$ . The interference order is also indicated. Spectral resolution is  $2 \text{ cm}^{-1}$ .

The injector was mounted in the MIDJet™ source as indicated in Fig. 4. The HF mixing nozzle for production of HF(v,J) from the  $\text{F} + \text{H}_2$  reaction was a 6 mm diameter stainless tube with four holes (0.5 mm diameter) spaced 1.5 cm apart. Hydrogen and He diluent were injected through this arrangement. The four holes produced supersonic flows of  $\text{H}_2$  from the exit plane to approximately 2 mm downstream of the holes. Fluorine atoms were produced with a 5 kW MIDJet™ discharge device using  $\text{SF}_6$  as the feedstock gas. Details of the water-cooled injector tube are shown in Fig. 5.

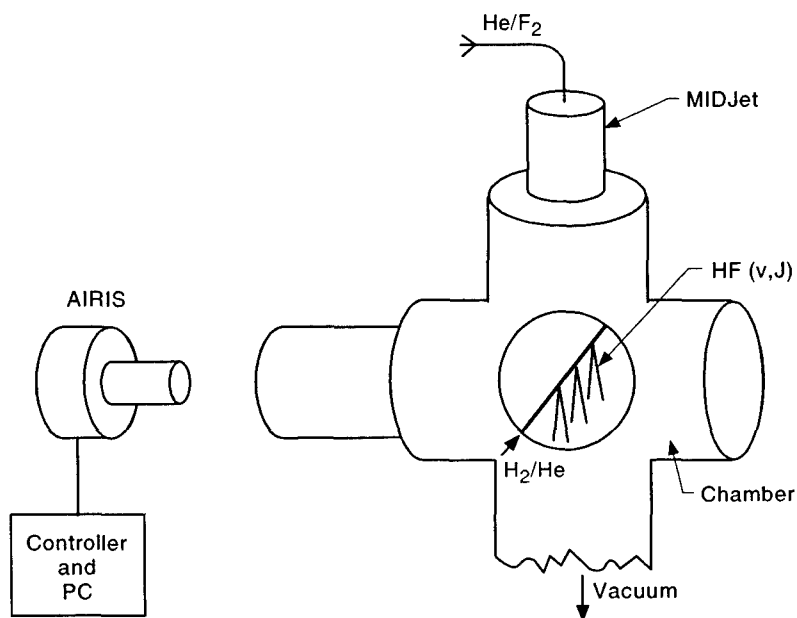


Fig. 4: Block diagram showing injector mounted in MIDJet™ device.

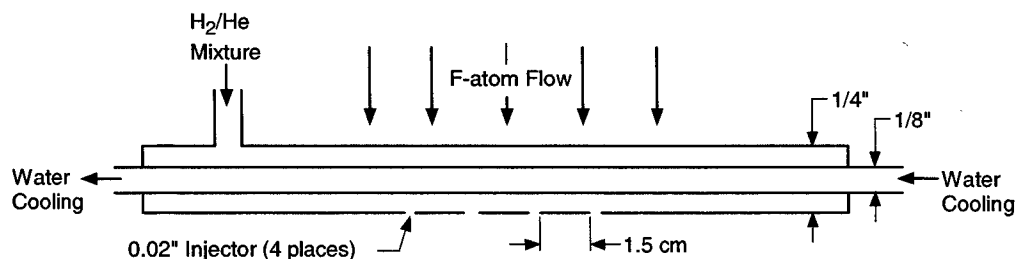


Fig. 5: H<sub>2</sub> injector used in the MIDJet™, HF production chamber.

### 2.3 Tests of AIRIS on HF flow chamber

The AIRIS device was positioned in front of a Cincinnati Electronics InSb IR camera equipped with a 4.1  $\mu\text{m}$  short-pass cold filter. We also used a bandpass filter to isolate the emission in the 2.6 to 2.9  $\mu\text{m}$  spectral region. The filter was placed directly in front of the camera. A camera zoom lens was used to focus the region of the HF injector, with the camera approximately 60 cm from the HF injector. In order to assure that the HF production chemistry made HF( $v,J$ ) we initially viewed the reaction zone with the FTIR spectrometer. The spectral region recorded between 2.65 and 2.9  $\mu\text{m}$  is shown in Fig. 6. Each feature can be assigned to an HF emission line and no other spectral features were observed. Even though the spectra are uncorrected for spectral response, it appears that the vibrational distribution is inverted with  $v=2$  having more population than  $v=1$ . Our source of HF appears to be an excellent surrogate for an actual HF laser reaction zone.

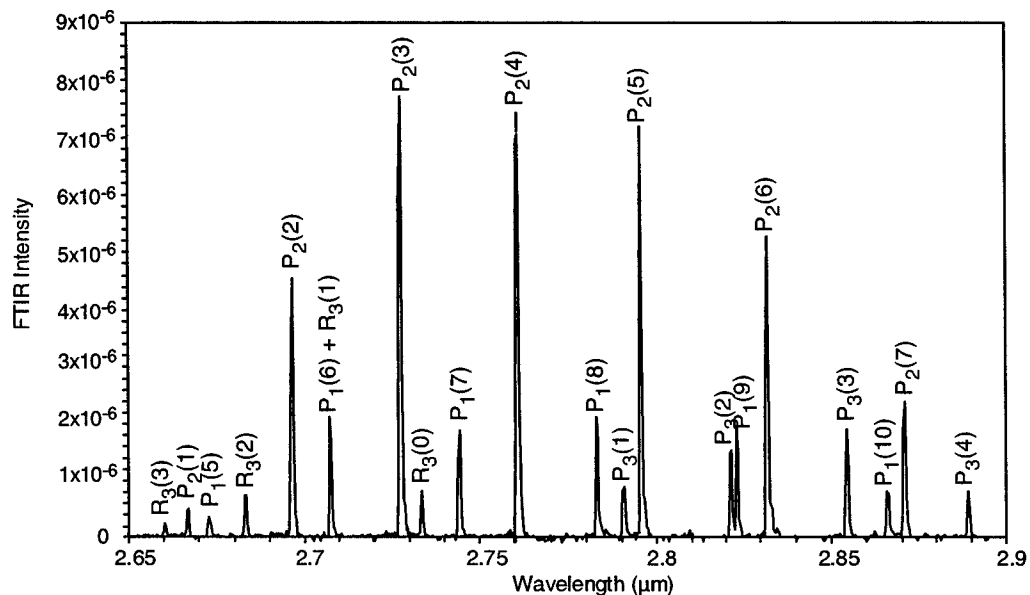


Fig. 6: FTIR spectrum of HF( $v,J$ ) emission recorded in our HF production chamber. Spectral resolution is 0.5  $\text{cm}^{-1}$ .

Fig. 7 shows an image of the HF flowfield obtained with the AIRIS. The image is emission from the P<sub>2</sub>(4) line near 2.76  $\mu\text{m}$ . The mixing of the F and H<sub>2</sub> downstream of the injection points is clearly evident. When the AIRIS is tuned off the P<sub>2</sub>(4) line (near the P<sub>1</sub>(7) line), the emission disappears, demonstrating the ability of AIRIS to spectrally isolate the HF emission lines. We have collected emission from numerous lines. Each image was also complemented by recording a full field image of a flat black body radiator at each wavelength. This allowed us to subsequently put each image on an absolute intensity basis. We also recorded a background image with the H<sub>2</sub> flow off. The raw images were corrected using the following procedure. First a background image was subtracted from each "raw" image. To correct each pixel for spectral response, each image was divided by the blackbody function at the appropriate wavelength of the image.

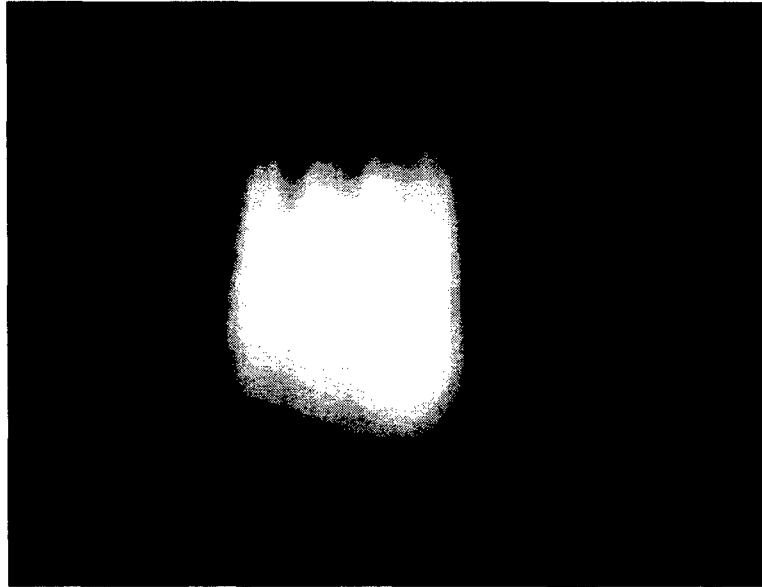


Fig. 7: AIRIS image of  $P_2(4)$  emission from chemically produced HF.

To further demonstrate that AIRIS can be used to study mixing phenomena in an HF laser, we performed an additional analysis on the flow field images. In Fig. 8 we show a section of the mixing region just downstream of the hydrogen injectors. Four planes: A,B,C, and D are shown. In Fig. 9 we show contours of these four planes and the progression of the mixing is evident as the flow progresses from A to D.

We also developed a strategy to image the population inversion in the flow field. When placed on an absolute scale, one can subtract images of the same scene recorded on sequential emission transitions to obtain these population inversion images. The method is outlined in Fig. 10. We used this approach to produce images of the inversion density of the flow field. Fig. 11 shows an image of the spatially resolved population inversion between the  $HF(v,J) = (2,4)$  and  $(1,5)$  levels. This key demonstration shows that AIRIS can be used to interrogate the small signal gain, a key parameter in HF lasers.

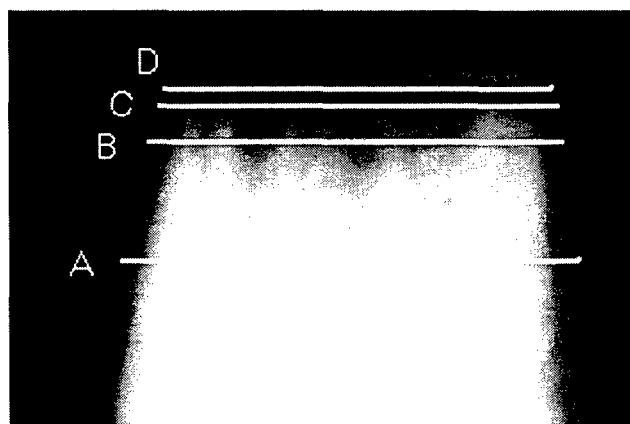


Fig. 8: HF emission from  $P_2(5)$  line. Analysis slices are indicated. Flow direction is down.

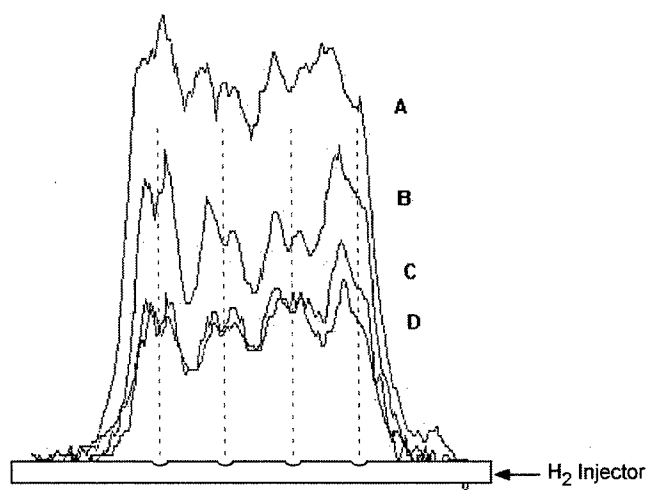


Fig. 9: Intensity profiles from image shown in Fig. 8.  
Flow direction is up.

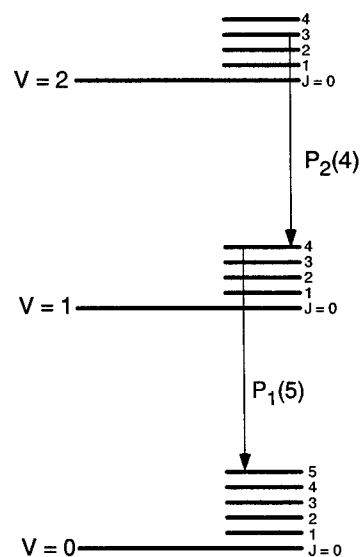


Fig. 10: Strategy for obtaining images of population inversion fields.

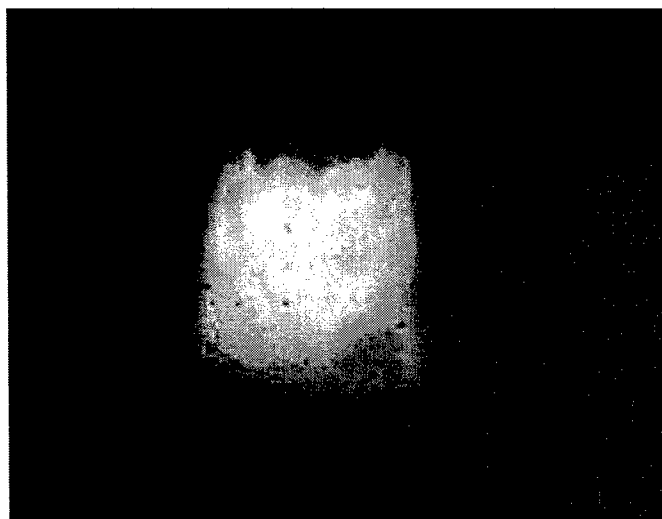


Fig. 11: Image of population inversion in PSI flowfield.

### 3. SUMMARY

We have described a novel diagnostic capable of probing chemically reacting flows for species concentration maps, mixing, and even population inversion maps. Using a subsonic flow reactor, we have obtained spatially and spectrally resolved maps of emission from excited HF molecules and 2-D images of the population inversion between two adjacent excited states in chemically produced HF. This device will be useful for a investigating a variety of parameters in the development of new, mid-IR chemical lasers.



## ACKNOWLEDGMENTS

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